# New Formula for Calculations of Scattering Cross-Sections According to Quantum Mechanics

Hasan Hüseyin Erbil

1. Physics Department, Faculty of ScienceEge University (Retired), Bornova-Izmir, Turkey

# Abstract:

We have calculated the general elastic and inelastic scattering differential and total cross-sections using a simple general solution of radial Schrödinger equation for a particle or particle current in a central field, generally. Before, we have obtained the general simple formulas of the scattering amplitudes and elastic, inelastic (no-elastic) and total scattering cross-sections. After, we have made some applications, numerically. In these applications, the barrier potentials are assumed to have centrifugal plus Coulomb potentials. With these potentials, the elastic, inelastic (absorption, radiation, particle detachment, particle capture, etc.) and total scattering cross-sections of different targets were calculated. Scattering cross-sections for  ${}_{2}^{3}$ He particles of three different energies on many targets, from  ${}_{4}^{9}Be$  to  ${}_{82}^{208}Pb$ , are calculated. The calculated results are compared with experimental results. The results calculated have given satisfactory agreement with the available experimental results. Then, when the experimental elastic and reaction cross sections are known, we calculated the width of the potential barrier and the coefficient of transmission of potential barrier. By taking thermal neutrons as incoming particles, the potential barrier transmission coefficients and barrier widths were calculated for many nuclei as examples.

*Keywords: Cross-sections, elastic scattering, inelastic (no-elastic), scattering theory, transmission coefficient* 

# INTRODUCTION

When a flowing particle or particle current is encountered with a potential energy barrier greater than its total energy, it cannot pass the potential barrier and return to its environment or disappear within the potential according to classical physics. However, the observations indicate that such a particle or particle current may pass the potential barrier. In quantum physics, this phenomenon is called tunneling. Studying the movement of the particle or particle current, including tunneling, is called scattering. The terms elastic and inelastic scattering are used in scattering theory. These terms are also measured by scattering cross sections. Elastic or inelastic (reaction or absorption) scattering and cross-sections are generally calculated according to the partial-wave expansion method or by a semi-classical method called WKB (Wentzel-Kramers-Brillouin) in nuclear physics. In these calculations, there are approximations, and the calculations are quite difficult and complex. All these approximations were made obligatory because the Schrödinger equation could not be solved exactly. Since the exact solution of the Schrödinger equation can now be made [1, 2], so it is not necessary to make these approximations. In this working, the differential elastic, inelastic and total scattering cross-sections were calculated using a simple general method developed for the solution of the radial SE (RSE) of a particle at the central field, without making any approach to the wave functions. First, we used our solution to calculate scattering amplitudes, particle currents, and the cross-section of scatterings from a general spherically symmetric potential containing attractive and repulsive parts. Then, the

scattering cross sections by several nuclei were calculated as examples. Then, the relationship between the cross sections and the tunneling or barrier transmission coefficient was calculated and made in several numerical applications. The calculated results were compared with the experimental results. All values were found to be in perfect agreement. It was then shown that if the experimentally measured cross sections are known, the coefficient of crossing the potential barrier and the width of the potential barrier can be found. Numerical applications were made.

### SCATTERING THEORY

Let us consider a spherical wave progressing at the direction of Oz axis from right to left and arriving to a central potential field, sitting at the origin of the Oxyz coordinate system. When we consider scattering, we shall assume that the interaction between the scattering particle and the scatter can be represented by an effective central potential energy function U(r), where r is the relative radial variable. The effective potential U(r) can include attractive and repulsive parts. Such a central potential is schematically represented in Figure 1. The total energy of the incoming particle beam is E, and the incoming particle beam can be represented by the spherical wave. This progressive spherical wave progress from right to left and arrives to the point  $r = r_1$  in Figure 1. We divide the potential region into three zones and examine the motion of particle beam into these three zones.

# **Conversion of Potential into Two Parts**

The effective potential contains both attractive (negative potential energy) and repulsive (barrier potential energy) parts. The energy of the incoming particle stream is always positive energy. To make the calculations easier and more understandable, it is more appropriate to make all the effective potential positive. If the potential is given as  $V(r) = V_0(r) - V_{00}$ ,  $[V_0(r) > 0 \text{ and } V_{00} > 0]$ , the effective potential is  $U(r) = V_0(r) - V_{00} + b/r^2 < 0$  in the bound states. Here,  $b/r^2$  is rotational energy, and  $-V_{00}$  is the depth of the potential well. Let us find the maximum and minimum values of this effective potential U(r). Let the roots of the equation U'(r) = 0,  $r_{m1}$  and  $r_{m2}$  be.  $r_0 = r_{m1}$  is the point where the effective potential largest value  $U(r_{m2}) = U_b$ . Let  $U_0 = U(r_0) - V_{00}$ . Thus,  $U(r) = V_0(r) - U_0 + b/r^2 < 0$  can be written. By solving this U(r) potential directly, energy values and wave functions can be found. However, if this potential is divided into two parts, with a well and an obstacle, there may be some convenience. The obstacle comes from rotational, gravity, Coulomb, and similar energies. Therefore, the U(r) potential can be written as the sum of two parts as follows:

$$U(r) = U_w(r) + U_b(r) ; [U_w(r) = V_0(r) - U_0 ; U_b(r) = b/r^2 + c/r]$$
(1)

Here, the  $U_w(r)$  potential is the vibration part of the U(r) potential, and the  $U_b(r)$  potential is total of the rotational and the other obstacle potential parts of the potential U(r). Here, c/r is the sum of gravity, Coulomb, and similar barrier potentials.  $U_0$  is the depth of the potential well. If the coordinate start is taken at the point  $(r_0, -U_0)$ , in this new coordinate system,  $U_b(r) = b/r^2 + c/r$  and  $U_w(r) = V_0(r)$ . Thus, the effective potential is written as follows:

$$U(r) = U_w(r) + U_b(r) ; [U_w(r) = V_0(r) ; U_b(r) = b/r^2 + c/r]$$
(2)

The graph of this potential is shown in Figure 1. (Shape of the U(r) in the coordinate system at  $(r_0, -U_0)$ . In this way, three domains I, II, III are obtained. Thus, by solving the equation (2), E energy values are found in the bound states. Here these solutions do not concern us. The barrier

potential  $U_b(r)$  causes scattering of the wave propagating from right to left. This potential interests us here.

# CALCULATION OF THE SCATTERING AMPLITUDES

Zone I is the region before the effective potential from where free particle comes; zones II, III are the effective potential regions where the particle beam is affected. These regions may include attractive and repulsive potential segments. In the scattering event, only the potential region  $U_2(r) = U_b(r)$  is effective. We assume that  $r = r_1$  and  $r = r_2$  at the interface between zone I and II, and zone II and III, respectively. The effective potential segments in the zones are represented as  $U_1(r), U_2(r)$  and  $U_3(r)$  according to the zone numbers. The central potential can be taken as zero at much far from the zone I so that the particle is free in that region and the effective potential is composed of only the centrifugal term due to the incoming particle angular momentum or spin. The Coulomb interaction potential should also be added to  $U_1(r)$  if that is available. The total energy of the incoming particle and the centrifugal term are always positive, and the latter is less than the former.



The radial function obtained from the general solution of the RSE is given as: [1, 2]

$$R(r) = F(r)/r ; F(r) = A e^{k r \pm i G(r)} + B e^{-k r \mp i G(r)}$$
(3)

- (a) For the case where  $E>U(r),\,\,k=i\,m_1\sqrt{E}\,,\,\,G(r)=i\,m_1\,\int\sqrt{U(r)}\,dr$
- (b) For the case where E < U(r),  $k = m_1 \sqrt{E}$ ,  $G(r) = m_1 \int \sqrt{U(r)} dr$

According to the functions given in Equations (3), the following functions are determined for the zones that are considered as follows:

In the zone I: E > 0,  $U_1(r) > 0$  and  $E > U_1(r)$ ;  $k = i m_1 \sqrt{E} = i K$ ;  $G_1(r) = i m_1 \int \sqrt{U_1(r)} dr = i Q_1(r)$ ;

In the zone II: E > 0,  $U_2(r) > 0$  and  $E < U_2(r)$ ;  $G_2(r) = m_1 \int \sqrt{U_2(r)} dr = Q_2(r)$ ;

# In the zone III:

 $E>0 \mbox{ and } E>U_3(r) \mbox{ ; } k=i \mbox{ } m_1 \sqrt{E}=i \mbox{ } K \mbox{ ; } G_3(r)=i \mbox{ } m_1 \int \sqrt{U_3(r)} \mbox{ } dr=i \mbox{ } Q_3(r) \mbox{ ; } K=m_1 \sqrt{E} \mbox{ ; } m_1=\sqrt{2 \mbox{ } m}/\hbar \mbox{ ; } Q_p(r)=m_1 \int \sqrt{U_p(r)} \mbox{ } dr \mbox{ , } (p=1,2,3)$ 

Under these circumstances, the radial wave functions in the three zones can be put in the forms below regarding the general functions given in Equations (3).

$$F_1(r) = A_1 e^{i K r - Q_1(r)} + B_1 e^{-i K r + Q_1(r)} ;$$
(4a)

$$F_2(r) = A_2 e^{K r \pm i Q_2(r)} + B_2 e^{-K r \mp i Q_2(r)} ;$$
(4b)

$$F_{3}(r) = A_{3}e^{-iKr \pm Q_{3}(r)} ; [Q_{1}(r) > 0, Q_{2}(r) > 0, Q_{3}(r) > 0]$$
(4c)

The potential in zone III can also be complex in some cases (usually called the optical potential). If  $U_3(r)$  is the optical potential, it can be written as follows:

$$U_{3}(r) = |U_{3}(r)|e^{i\phi} = U_{31}(r) + i U_{32}(r) = \sqrt{U_{31}^{2}(r) + U_{32}^{2}(r)} e^{i\phi}$$
(5a)

 $\tan(\emptyset) = \frac{U_{32}(r)}{U_{31}(r)}$ ,  $\emptyset = \arctan\left[\frac{U_{32}(r)}{U_{31}(r)}\right]$ ;  $k = i m_1 \sqrt{E} = i m_1 \sqrt{-|E|} = K$ 

$$Q_3(r) = \int \sqrt{|U_3(r)|} \, dr = m_1 \int \sqrt{\sqrt{U_{31}^2(r) + U_{32}^2(r)}} \, dr = m_1 \int \sqrt[4]{U_{31}^2(r) + U_{32}^2(r)} \, dr$$
(5b)

In Equations (4a-4c), the functions  $Q_p(r)$  can also be written briefly as follows:

$$Q_p(r) = m_1 \int \sqrt{|U_p(r)|} dr$$
,  $[p = 0, 1, 2, 3]$  (5c)

The terms of containing ( $A_1$  and  $B_1$ ) coefficients in the functions of the Equation (4a) give outgoing wave and incoming waves, respectively. We assume that the amplitude of incoming wave at the boundary of zone I and II is constant. The second (4b) and the third (4c) functions represent the states of the wave in the effective region of the potential. The (4c) function represents the wave passing from region (II) to region (III). Applying the continuity conditions on  $F_p(r_j)$  and  $F'_p(r_j)$ , [p, j = 1, 2, 3] functions, the coefficients  $A_1$  and  $B_1$  in Equations (4a–4c) can be determined. These conditions at the boundary points of the three zones can be written in the following form:

$$F_{1}(r_{1}) = F_{2}(r_{1}); F_{1}'(r_{1}) = F_{2}'(r_{1}); F_{2}(r_{2}) = F_{3}(r_{2}); F_{2}'(r_{2}) = F_{3}'(r_{2}); Q_{p}'(r_{j}) = K, (p, j = 1, 2, 3)$$
(6)

The coefficients  $A_1$ ,  $A_2$ ,  $B_2$ ,  $A_3$  in the functions given in Equations (4a–4c) can be found by solving four linear equations, which can be obtained by using the conditions given in Equation (6) for each of the functions given in Equations (4a–4c). These coefficients are obtained depending on the  $B_1$  coefficient. The essential coefficients for the scattering cross section are  $A_1$  and  $A_3$  as described below. Therefore, there is no need to give other coefficients here. The  $A_1$  and  $A_3$  coefficient, which is obtained from four equations, is computed by considering the lower and upper signs in the exponential expressions in Equations (4a-4c). With these coefficients, the tunnel passing coefficient can be recalculated. We have calculated these coefficients, but there is no need to give them here. Because, as can be seen below, these coefficients are not needed to calculate the scattering cross sections. Now, let us explain this situation below:

The terms with  $A_1$  and  $B_1$  in the functions given in Equation (4a) representing the outgoing and incoming waves respectively at the point  $r = r_1$ . So, the  $r_1$  value is obtained by solving the equation  $E = U_b(r)$ . Thus, the wave functions arriving and scattered at the  $r = r_1$  and passing through to the point  $r = r_2$  are as follows:

$$C_{s}(r_{1}) = A_{1} e^{\pm Q_{1}(r_{1})}, \text{ (scattering amplitude);} R_{s}(r) = \frac{F_{s}(r)}{r} = C_{s}(r_{1}) \frac{e^{i K r}}{r} = A_{1} e^{\pm Q_{1}(r_{1})} \frac{e^{i K r}}{r}$$
(7a)

$$C_{c}(r_{1}) = B_{1} e^{\pm Q_{1}(r_{1})}, \text{ (incoming amplitude);} R_{c}(r) = \frac{F_{c}(r)}{r} = C_{c}(r_{1}) \frac{e^{-iKr}}{r} = B_{1} e^{\pm Q_{1}(r_{1})} \frac{e^{-iKr}}{r}$$
(7b)

$$C_{p}(r_{2}) = A_{3} e^{\pm Q_{3}(r_{2})}, \text{ (passing amplitude);}$$

$$R_{p}(r) = \frac{F_{p}(r)}{r} = C_{p}(r_{2}) \frac{e^{-iKr}}{r} = A_{3} e^{\pm Q_{3}(r_{2})} \frac{e^{-iKr}}{r}$$
(7c)

The functions (7a-7c) represent scattering, incoming and transmission waves, respectively.

# **Calculation of Particle Currents**

Using the (7a-7c) functions and the equation  $J(r) = \frac{\hbar}{2 \text{ m i}} \left[ R^*(r) \frac{dR(r)}{dr} - R(r) \frac{dR^*(r)}{dr} \right]$ , the current density expression, the current densities for these three functions are found as follows:

| $J_{s} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m} C_{s} C_{s}^{*} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m}  C_{s} ^{2}$              | (scattering current density) | (8a) |
|--|------------------------------|------|
| $J_{c} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m} C_{c} C_{c}^{*} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m}  C_{c} ^{2}$              | (incoming current density)   | (8b) |
| $J_{p} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m} C_{p} C_{p}^{*} = \frac{1}{r_{1}^{2}} \frac{\hbar K}{m} \left  C_{p} \right ^{2}$ | (passing current density)    | (8c) |

# CALCULATIONS OF SCATTERING CROSS-SECTIONS

# **Calculation of Differential Elastic Scattering Cross-Section**

The probability per unit differential surface of a sphere of radius  $r_1$ , that an incident particle is scattered into the differential surface area on the sphere of radius  $r_1$ ,  $dS = r_1^2 d\Omega$ ,  $[d\Omega = sin(\theta) d\theta d\phi]$  is expressed as the ratio of the scattered current to the incident current, that is:

$$\frac{d\sigma_s}{dS} = \frac{d\sigma_s}{r_1^2 d\Omega} = \frac{J_s(r_1)}{J_c(r_1)} \rightarrow \frac{d\sigma_s}{d\Omega} = \frac{J_s(r_1)}{J_c(r_1)} r_1^2$$
(9)

The differential elastic cross-section can be expressed in a simple form by putting Equations (8) into Equation (9) as follows:

$$\frac{d\sigma_s}{d\Omega} = \frac{C_s(r_1) C_s^*(r_1)}{C_c(r_1) C_c^*(r_1)} r_1^2 = \frac{|C_s(r_1)|^2}{|C_c(r_1)|^2} r_1^2 = \frac{J_s(r_1)}{J_c(r_1)} r_1^2$$
(10)

Since the scattering is azimuthally symmetrical, the angle  $\phi$  can be integrated out so that the expression given in Equation (10) can be written as follows:

$$\frac{d\sigma_s}{d\theta} = 2 \pi \frac{J_s(r_1)}{J_c(r_1)} r_1^2 \sin(\theta) = 2 \pi \frac{|C_s(r_1)|^2}{|C_c(r_1)|^2} r_1^2 \sin(\theta)$$
(11)

The expression (11) shows the elastic scattering differential cross sections in the angle  $d\theta$  which is usually measured experimentally.

# Calculation of Differential Inelastic or Reaction (No-Elastic) Cross-Section

Differential reaction (capture of particle, emission of particle, inelastic collision...) cross- section per the solid angle can be found through the difference between the incoming current and the outgoing current divided by the former. By analogy with Equation (11), the differential reaction cross-section can be expressed as follows:

$$\frac{d\sigma_{\rm r}}{d\theta} = 2 \pi \frac{[J_{\rm c}(r_1) - J_{\rm s}(r_1)]}{J_{\rm c}(r_1)} r_1^2 \sin(\theta) = 2 \pi \frac{[|C_{\rm c}(r_1)|^2 - |C_{\rm s}(r_1)|^2]}{|C_{\rm c}(r_1)|^2} r_1^2 \sin(\theta)$$
(12)

#### **Calculation of Total Cross Sections**

The total elastic scattering cross section is the total probability to be elastic scattered in any direction and it can be determined through the integral of differential cross-section given in Equation (11) as follows:

$$\sigma_{s} = \int d\sigma_{s} = \int \frac{d\sigma_{s}}{d\Omega} d\Omega = \iint \frac{J_{s}(r_{1})}{J_{c}(r_{1})} r_{1}^{2} \sin(\theta) d\theta d\phi = 4 \pi r_{1}^{2} \frac{J_{s}(r_{1})}{J_{c}(r_{1})} = 4 \pi r_{1}^{2} \frac{|C_{s}(r_{1})|^{2}}{|C_{c}(r_{1})|^{2}}$$
(13)

By analogy with Equation (11), the total reaction cross-section can be expressed as follows:

$$\sigma_{\rm r} = 4 \,\pi \,r_1^2 \, \frac{[J_{\rm c}(r_1) - J_{\rm s}(r_1)]}{J_{\rm c}(r_1)} = 4 \,\pi \,r_1^2 \, \left(1 - \frac{J_{\rm s}(r_1)}{J_{\rm c}(r_1)}\right) = 4 \,\pi \,r_1^2 \, \left(1 - \frac{|\mathsf{C}_{\rm s}(r_1)|^2}{|\mathsf{C}_{\rm c}(r_1)|^2}\right) = 4 \,\pi \,r_1^2 - \sigma_{\rm s} \tag{14}$$

In Equation (12), it is seen that if  $J_s(r_1) = J_c(r_1)$ , then  $\sigma_r = 0$ , full-elastic scattering; if  $J_s(r_1) > J_c(r_1)$ , then  $\sigma_r < 0$ , it is taken out of the particle from the target (emission of particle from target) and if  $J_s(r_1) < J_c(r_1)$ , then  $\sigma_r > 0$ , it is captured (absorbed) the particle by the target.

The total scattering cross-section, including all process [elastic plus reaction (all no-elastic events)]:

$$\sigma_{t} = \sigma_{s} + \sigma_{r} = 4 \pi r_{1}^{2} \frac{J_{s}(r_{1})}{J_{c}(r_{1})} + 4 \pi r_{1}^{2} \frac{[J_{c}(r_{1}) - J_{s}(r_{1})]}{J_{c}(r_{1})} = 4 \pi r_{1}^{2}$$
(15)

Then, the cross-sections  $\sigma_s$ ,  $\sigma_r$ ,  $\sigma_t$  can be expressed through the  $C_s(r_1)$  coefficient given above.

# RELATIONSHIP BETWEEN SCATTERING CROSS SECTIONS AND POTENTIAL BARRIER TRANSMISSION COEFFICIENT (TRANSMISSION COEFFICIENT) T

It is also possible to easily calculate the scattering cross-sections in terms of the potential barrier transmission coefficient (T), which are calculated by the amplitudes of the waves and given by the formulas (13-15). But there is no need to calculate amplitudes and particle currents here. Because the scattering cross sections can be easily calculated based on the coefficient of crossing the potential barrier. Now, let us calculate the scattering cross sections depending on the coefficient of crossing the potential barrier.

Incoming particle current  $J_c$ , elastic scattering particle current  $J_s$ , transmission or remaining in the potential barrier (inelastic or reaction) particle current  $J_r$ ; let the total elastic scattering cross section  $\sigma_s$ , the total reaction cross section  $\sigma_r$ , and the total scattering cross section  $\sigma_t$  be. By putting  $J_r = T J_c$  in expressions (13-15), the following expressions are obtained:

$$\sigma_{\rm s} = 4 \,\pi \,r_1^2 \,\frac{J_{\rm c} - J_{\rm r}}{J_{\rm c}} = 4 \,\pi \,r_1^2 \,\left(1 - \frac{J_{\rm r}}{J_{\rm c}}\right) = 4 \,\pi \,r_1^2 \,\left(1 - \frac{T \,J_{\rm c}}{J_{\rm c}}\right) = 4 \,\pi \,r_1^2 \,\left(1 - T \,\right) \tag{16}$$

$$\sigma_{\rm r} = 4 \,\pi \,r_1^2 \,\frac{J_{\rm c} - J_{\rm s}}{J_{\rm c}} = 4 \,\pi \,r_1^2 \,\frac{J_{\rm c} - (J_{\rm c} - J_{\rm r})}{J_{\rm c}} = 4 \,\pi \,r_1^2 \,\frac{J_{\rm r}}{J_{\rm c}} = 4 \,\pi \,r_1^2 \,\frac{T \,J_{\rm c}}{J_{\rm c}} = 4 \,\pi \,r_1^2 \,T \tag{17}$$

$$\sigma_{\rm t} = \sigma_{\rm s} + \sigma_{\rm r} = 4 \,\pi \,r_1^2 \tag{18}$$

 $(J_c, J_s, J_r)$  are incoming, scattering, reaction currents, respectively. Here, T is the tunneling probability coefficient (or transmission coefficient of potential barrier) is given by the following formula [1-6]:

$$T = \frac{2}{\cosh[2 \text{ K d}] + \cos(2 \text{ P})}$$

Here, the width of the potential barrier  $d = r_1 - r_2$ ,  $K = m_1 \sqrt{|E|}$ ,  $m_1 = \sqrt{2 m}/\hbar$ , E energy, and  $P = Q_2(r_1) - Q_2(r_2)$ . If  $Q_2(r)$  is pair function, P = 0. If  $Q_2(r)$  is not pair function,  $P = \text{Real}[Q_2(r_1) - Q_2(r_2)]$  zero or approximately zero can take. So, if P = 0, the following coefficient of transmission is obtained:

$$T(d_2) = \frac{2}{1 + \cosh[2 K(E)d_2(E)]}, d_2 = r_1 - r_2.$$
 If  $d_2 = 0$ , then  $T = 1$  (19)

It is easier to calculate T, which obviously does not depend on the shape of the potential barrier. It can be seen from (16-18) that the scattering cross sections depend on the penetration coefficient  $T(d_2)$  and  $r_1$ . Calculating this coefficient T is easier than calculating amplitudes. In fact, the T coefficient is also obtained by calculating the scattering amplitudes described above. As a result, the scattering cross sections are simply.

$$\sigma_{s} = 4 \pi r_{1}^{2} 10 \left[ 1 - T(d_{2}(E)) \right] = 40 \pi r_{1}^{2} \left[ 1 - T(d_{2}(E)) \right]$$
<sup>(20)</sup>

$$\sigma_{\rm r} = 4 \,\pi \,r_1^2 \,10 \,T \big( d_2(E) \big) = 40 \,\pi \,r_1^2 \,T \big( d_2(E) \big) \tag{21}$$

 $\sigma_t = \sigma_s + \sigma_r = 4 \pi r_1^2 * 10 = 40 \pi r_1^2$ 

If  $r_1$  and  $d_2$  are taken as fermi (fm) in equations (20-22), the scattering cross sections will be millibarn (mb). The factor of 10 in these equations comes from taking such units. It can be seen from these formulas given in Equations (20-22) that the scattering cross-sections ( $\sigma_s$ ,  $\sigma_r$  and  $\sigma_t$ ) depend on the total energy E [with K(E),  $r_1(E)$  and  $d_2(E)$ ]. Here,  $r_1$  can be considered as impact or collision parameter, classically.

# EXAMPLES OF THE CALCULATION OF SCATTERING CROSS-SECTION Model Potentials and Their Some Ingredients

To calculate a scattering cross-section, a model potential should be considered. We consider the potential for scattering in Figure 1. As can be seen from the (20-22) formulas, wave functions are not needed to calculate the scattering cross sections. Therefore, there is no need to know the exact shapes of the potentials. It is sufficient to calculate only the  $r_1$  and  $r_2$  coordinates. Here as example, we consider two cases: (1) Rectangle potential as  $U_3$  potential segment, and barrier potential  $U_b$  as  $U_2$  potential segment (centrifugal potential plus Coulomb potential). (2) Harmonic oscillator potential as  $U_3$  potential segment, and barrier potential  $U_b$  as potential  $U_2$  (centrifugal potential plus Coulomb potential). The potential zones are defined in Figure 1. The scattering affects only relative motion. The scattering cross-section of the incoming (incident or projectile) particle depends on the relative energy  $E_r = M_t E_L/(M_p + M_t)$ , where  $M_p$  and  $M_t$  respectively mass of incident (projectile) and target particles;  $E_L$ . Laboratory energy; and  $E_r$ , relative energy.

# Case 1. Rectangle Potential As $\rm U_3$ Potential Segment and Barrier Potential $\rm U_b$ As $\rm U_2$ Potential Segment

We have taken  $r_2 = R_0 (A_p^{1/3} + A_t^{1/3})$  in potential segment  $U_3$ , and  $U_b(r) = b/r^2 + C_c/r$  as potential segment  $U_2$ , where  $A_p$  and  $A_t$  are the mass numbers of the projectile and the target, respectively.  $R_0$  is a parameter. The positive root of the equation  $U_2(r) = U_b(r) = E_r$  is  $r_{11} = C_c + \sqrt{C_c^2 + 4 b E_r}/(2 E_r)$ . Then,  $r_1 = r_2 + r_{11}$ . So,  $r_1 - r_2 = d_2(E) = r_{11}$  is the width of the potential barrier. The zones and  $r_k$ , (k = 1, 2) values are shown in Figure 1.

 $V_S(r)=b/r^2$  , centrifugal potential ;  $~~b=\hbar^2$  J (J + 1)/(2  $M_r)$  ,  $M_r\,$  reduced mass, J relative total angular momentum.

 $V_c(r) = C_c/r$ , Coulomb potential,  $C_c = (Z_p e)(Z_t e) = Z_p Z_t e^2$ ,  $Z_p$  and  $Z_t$  are charge number of projectile and target, respectively. And e is the unit electric charge.

It is seen from Equations (20-22) that  $\sigma_t$  depends only on the  $r_1$  value, although the  $\sigma_s$  and  $\sigma_r$  cross sections depend on the  $r_1$  and T quantities. The  $r_2$  quantity depends on the  $R_0$  parameter. Even though  $\sigma_s$  and  $\sigma_r$  have changed with the T and  $r_1$ ,  $\sigma_t = \sigma_s + \sigma_r$  depend on only  $r_1$ . In other words, the total cross-section does not depend on the T. So,  $R_0$  parameter can be obtained from the solution of the equation  $4\pi r_1^2 * 10 = \sigma_t^{exp}$  as follows, ( $\sigma_t^{exp}$  is experimental total cross-section):

$$R_{0} = \frac{-\sqrt{\pi} \ 10 \left[C_{c} + \sqrt{C_{c}^{2} + 4 \ b \ E_{r}}\right] + E_{r} \ \sqrt{10 \ \sigma_{t}^{exp}}}{20 \ E_{r} \sqrt{\pi} \left[\sqrt[3]{A_{p}} + \sqrt[3]{A_{t}}\right]}$$

(22)

|                                       |                                  |                            |                                     |                            | comparison w                       |                          |                          |                       |                          |
|---------------------------------------|----------------------------------|----------------------------|-------------------------------------|----------------------------|------------------------------------|--------------------------|--------------------------|-----------------------|--------------------------|
| Xn[Z, N]<br>(Target)                  | E <sub>L</sub> (MeV)<br>He (2,3) | <b>r</b> <sub>2</sub> (fm) | <b>r</b> <sub>1</sub> ( <b>fm</b> ) | <b>d</b> <sub>2</sub> (fm) | <b>T</b> ( <b>d</b> <sub>2</sub> ) | $\sigma_s^{cal}$<br>(mb) | $\sigma_r^{cal}$<br>(mb) | $\sigma_t^{cal}$ (mb) | $\sigma_t^{exp}$<br>(mb) |
| Be (4,9)                              | 96.4                             | 2.13126                    | 2.53101                             | 0.399748                   | 0.349472                           | 524                      | 281                      | 805                   | 805                      |
| Be (4,9)                              | 137.8                            | 1.98812                    | 2.30905                             | 0.320928                   | 0.489133                           | 342                      | 328                      | 670                   | 670                      |
| Be (4,9)                              | 167.3                            | 1.94451                    | 2.23016                             | 0.285641                   | 0.449812                           | 344                      | 281                      | 625                   | 625                      |
| C (6,12)                              | 96.4                             | 2.11525                    | 2.53885                             | 0.423602                   | 0.274485                           | 588                      | 222                      | 810                   | 810                      |
|                                       | 137.8                            | 2.04314                    | 2.33683                             | 0.333830                   | 0.42318                            | 410                      | 300                      | 710                   | 710                      |
| C (6,12)<br>C (6,12)                  | 167.3                            | 1.9711                     | 2.26556                             | 0.294453                   | 0.389204                           | 394                      | 251                      | 645                   | 645                      |
| C (0,12)                              | 107.5                            | 1.9711                     | 2.20330                             | 0.294455                   | 0.389204                           | 594                      | 231                      | 045                   | 045                      |
| O (8,16)                              | 96.4                             | 2.33304                    | 2.78546                             | 0.452419                   | 0.108278                           | 869                      | 106                      | 975                   | 975                      |
| O (8,16)                              | 137.8                            | 2.25012                    | 2.60079                             | 0.350669                   | 0.315005                           | 582                      | 268                      | 850                   | 850                      |
| O (8,16)                              | 167.3                            | 2.21638                    | 2.52313                             | 0.306753                   | 0.330808                           | 535                      | 265                      | 800                   | 800                      |
| Si (14,28)                            | 96.4                             | 2.57607                    | 3.15392                             | 0.577846                   | 0.058062                           | 1177                     | 73                       | 1250                  | 1250                     |
| Si (14,28)                            | 137.8                            | 2.5937                     | 3.02513                             | 0.431427                   | 0.234463                           | 880                      | 270                      | 1250                  | 1250                     |
| · · · · · · · · · · · · · · · · · · · | 167.3                            | 2.5957                     | 2.91119                             | 0.431427                   | 0.184194                           | 869                      | 196                      | 1065                  |                          |
| Si (14,28)                            | 107.5                            | 2.54117                    | 2.91119                             | 0.370019                   | 0.184194                           | 809                      | 190                      | 1005                  | 1065                     |
| Ca (20,40)                            | 96.4                             | 2.56153                    | 3.28976                             | 0.728229                   | 0.006241                           | 1352                     | 8                        | 1360                  | 1360                     |
| Ca (20,40)                            | 137.8                            | 2.65994                    | 3.19154                             | 0.531601                   | 0.095339                           | 1158                     | 122                      | 1280                  | 1280                     |
| Ca (20,40)                            | 167.3                            | 2.67211                    | 3.12222                             | 0.450103                   | 0.091308                           | 1113                     | 112                      | 1225                  | 1225                     |
| Ni (28,58)                            | 96.4                             | 2.72392                    | 3.66723                             | 0.943309                   | 0.000722                           | 1689                     | 1                        | 1690                  | 1690                     |
| Ni (28,58)                            | 137.8                            | 2.72392                    | 3.53464                             |                            | 0.032315                           |                          |                          |                       |                          |
|                                       | 167.3                            | 2.85255                    | 3.42022                             | 0.677288                   | 0.031998                           | 1519<br>1423             | 51<br>47                 | 1570<br>1470          | 1570<br>1470             |
| Ni (28,58)                            | 107.5                            | 2.65255                    | 5.42022                             | 0.507000                   | 0.031998                           | 1425                     | 47                       | 1470                  | 1470                     |
| Ni (28,60)                            | 96.4                             | 2.72005                    | 3.6618                              | 0.941755                   | 0.000605                           | 1684                     | 1                        | 1685                  | 1685                     |
| Ni (28,60)                            | 137.8                            | 2.90321                    | 3.57938                             | 0.676173                   | 0.032315                           | 1558                     | 52                       | 1610                  | 1610                     |
| Ni (28,60)                            | 167.3                            | 2.89971                    | 3.46644                             | 0.566731                   | 0.031998                           | 1462                     | 48                       | 1510                  | 1510                     |
| Sp (EQ 112)                           | 96.4                             | 2.54198                    | 4.1122                              | 1.570220                   | 1.6668*10 <sup>-6</sup>            | 2125                     | 0                        | 2125                  | 2125                     |
| Sn (50,112)                           | 137.8                            | 2.95942                    | 4.06843                             |                            | 0.001269                           | 2123                     | 0                        | 2080                  | 2080                     |
| Sn (50,112)<br>Sn (50,112)            | 167.3                            | 3.14889                    | 4.06843                             | 1.109010<br>0.919543       | 0.001209                           | 2077                     | 3                        | 2080                  | 2080                     |
| 311 (30,112)                          | 107.5                            | 5.14005                    | 4.00645                             | 0.919343                   | 0.001300                           | 2077                     | 5                        | 2080                  | 2080                     |
| Sn (50,116)                           | 96.4                             | 2.65792                    | 4.22672                             | 1.5688                     | 1.20939*10 <sup>-6</sup>           | 2245                     | 0                        | 2245                  | 2245                     |
| Sn (50,116)                           | 137.8                            | 3.02832                    | 4.13632                             | 1.108                      | 0.00126874                         | 2147                     | 3                        | 2150                  | 2150                     |
| Sn (50,116)                           | 167.3                            | 3.21761                    | 4.13632                             | 0.918711                   | 0.00136031                         | 2147                     | 3                        | 2150                  | 2150                     |
| Sn (E0 110)                           | 96.4                             | 2.72861                    | 4.29674                             | 1.56813                    | 1.0125*10 <sup>-6</sup>            | 2220                     | Ω                        | 2320                  | 2320                     |
| Sn (50,118)<br>Sn (50,118)            | 96.4<br>137.8                    | 3.12389                    | 4.29674                             | 1.10753                    | 0.00009892                         | 2320<br>2250             | 0                        | 2320                  | 2320                     |
| Sn (50,118)<br>Sn (50,118)            | 167.3                            | 3.24676                    | 4.16508                             | 0.918316                   | 0.00136031                         | 2250                     | 3                        | 2250                  | 2230                     |
| 311 (30,118)                          | 107.5                            | 5.24070                    | 4.10508                             | 0.916510                   | 0.00130031                         | 21/7                     | 5                        | 2100                  | 2180                     |
| Sn (50,120)                           | 96.4                             | 2.69673                    | 4.26421                             | 1.56747                    | 1.20054*10 <sup>-6</sup>           | 2285                     | 0                        | 2285                  | 2285                     |
| Sn (50,120)                           | 137.8                            | 3.10551                    | 4.21257                             | 1.10707                    | 0.00126874                         | 2227                     | 3                        | 2230                  | 2230                     |
| Sn (50,120)                           | 167.3                            | 3.24715                    | 4.16508                             | 0.917934                   | 0.00136031                         | 2177                     | 3                        | 2180                  | 2180                     |
| C (FO 15.1)                           | 00.0                             | 0 - 4455                   | 4.040.51                            | 4 5 6 6 5 5                | 4 202254125                        | 200-                     | _                        | 200-                  | 2007                     |
| Sn (50,124)                           | 96.4                             | 2.74438                    | 4.31061                             | 1.56623                    | 1.20735*10-6                       | 2335                     | 0                        | 2335                  | 2335                     |
| Sn (50,124)                           | 137.8                            | 3.09693                    | 4.20312                             | 1.10619                    | 0.00126874                         | 2217                     | 3                        | 2220                  | 2220                     |
| Sn (50,124)                           | 167.3                            | 3.22872                    | 4.14593                             | 0.917206                   | 0.00136031                         | 2157                     | 3                        | 2160                  | 2160                     |
| Pb(82,208)                            | 96.4                             | 2.18335                    | 4.69075                             | 2.50741                    | 1.4303*10 <sup>-10</sup>           | 2765                     | 0                        | 2765                  | 2765                     |
|                                       |                                  |                            |                                     | 1                          |                                    | -                        |                          | -                     | -                        |
| Pb (82,208)                           | 137.8                            | 3.00165                    | 4.76231                             | 1.76066                    | 9.54594*10 <sup>-6</sup>           | 2850                     | 0                        | 2850                  | 2850                     |

 Table 1. [He [2,3] + Xn [Z,N] Cross-sections comparison with those measured (case 1)

Thus,  $r_1$  and  $r_2$  values are calculated, and  $d_2$  and  $T(d_2)$  values are found. With these values,  $\sigma_s$ ,  $\sigma_r$  and  $\sigma_t$  values are calculated. The mass values of the nuclei and some conversion factors and the values of the universal constants used were taken from [7, 8]. We have taken in the calculations the following values:  $e^2 = 1.439976$  MeV fm ;  $M_u = 931.502$  MeV/ $c^2$ ;  $\hbar c = 197.329$  MeV fm. The cross-sections at three different energies of He[2,3] have been calculated for many different targets. The calculated cross-sections have been compared with those measured taken from [9-11]. The comparisons are made in the way that is described above and given in Table 1. In this table: Xn [Z, N] target;  $E_L$  laboratory energy of projectile;  $\sigma_r^{cal}$ ,  $\sigma_s^{cal}$ ,  $\sigma_t^{cal}$  calculated reaction, elastic total cross-sections;  $\sigma_t^{exp}$  experimental measured total cross-section. There is no need for relative angular momentums here. Because the individual total angular momentum of the target particles, except Be (4,9), is zero.

# Case 2. Harmonic Oscillator Potential As U<sub>3</sub> Potential, Barrier Potential U<sub>b</sub> As Potential U<sub>2</sub> (Centrifugal Potential Plus Coulomb Potential).

We have taken the harmonic oscillator potential  $V(r) = \frac{1}{2} M_r \omega^2 r^2$  as potential segment  $U_3$ , and  $U_b(r) = b/r^2 + C_c/r$  as potential segment  $U_2$ , where  $M_r$  and  $\omega$  are the reduced mass of the projectile and the target, and a parameter, respectively. The positive root of the equation  $V(r) = E_r$  is  $r_2 = \sqrt{2 E_r / (M_r \omega^2)}$ , and the positive root of the equation  $U_b(r) = E_r$  is  $r_{11} = C_c + \sqrt{C_c^2 + 4 b E_r} / (2 E_r)$ . Then,  $r_1 = r_2 + r_{11}$ . So,  $r_1 - r_2 = d_2(E) = r_{11}$  is the width of the potential barrier. The zones and  $r_k$ , (k = 1, 2) values are shown in Figure 1.

 $V_S(r)=b/r^2$  , centrifugal potential ;  $\,b=\hbar^2\,J\,(J+1)/(2\,M_r)$  ,  $\,M_r\,$  reduced mass, J relative total angular momentum.

 $V_c(r) = C_c/r$ , Coulomb potential,  $C_c = (Z_p e)(Z_t e) = Z_p Z_t e^2$ ,  $Z_p$  and  $Z_t$  are charge number of projectile and target, respectively. And e is the unit electric charge.

It is seen from Equations (20-22) that  $\sigma_t$  depends only on the  $r_1$  value, although the  $\sigma_s$  and  $\sigma_r$  cross sections depend on the  $r_1$  and T quantities. The  $r_2$  quantity depends on the  $\omega$  parameter. Even though  $\sigma_s$  and  $\sigma_r$  have changed with the T and  $r_1$ ,  $\sigma_t = \sigma_s + \sigma_r$  depend on only  $r_1$ . In other words, the total cross-section does not depend on the T. So,  $\omega$  parameter can be obtained from the solution of the equation  $4\pi r_1^2 * 10 = \sigma_t^{exp}$  as follows ( $\sigma_t^{exp}$  is experimental total cross-section):

$$\omega = \frac{4\left(-5\sqrt{2} E_{r}\left(C_{c} + \sqrt{C_{c}^{2} + 4 b E_{r}}\right)\sqrt{E_{r}M_{r}} \pi + \sqrt{5\pi}\sqrt{E_{r}^{5}M_{r}\sigma_{t}^{exp}}\right)}{M_{r}\left(20\left(C_{c}^{2} + 2 b E_{r}\right)\pi + 20 C_{c}\sqrt{C_{c}^{2} + 4 b E_{r}} \pi - E_{r}^{2}\sigma_{t}^{exp}\right)}$$

After that, the procedures in case 1 were performed exactly and the results are given in Table 2. Experimental cross section values were taken from [9, 11].

| le [2,3]                         | + xn z   | I, NJ Cro   | oss-sections   |  |  |   |                                       | ase 2)   |
|----------------------------------|--|---|--|--|--|---|---------------------------------------|--|
| E <sub>L</sub> (MeV)<br>He (2,3) | <b>r</b> <sub>2</sub> ( <b>fm</b> )  | <b>r</b> <sub>1</sub> (f <b>m</b> )   | <b>d</b> <sub>2</sub> (fm)   | <b>T</b> ( <b>d</b> <sub>2</sub> )   | σ <sub>s</sub> <sup>cal</sup><br>(mb)  | $ \begin{array}{c} \sigma_r^{cal} \\ (mb) \end{array} $   | σ <sub>T</sub> <sup>cal</sup><br>(mb) | $ \begin{array}{c} \sigma^{exp}_T \\ (mb) \end{array} $  |
| 96.4                             | 213.126  | 253.101   | 0.399748   | 0.349472   | 524  | 281   | 805                                   | 805  |
| 137.8                            | 198.812  | 230.905   | 0.320928   | 0.489133   | 342  | 328   | 670                                   | 670  |
| 167.3                            | 194.451  | 223.016   | 0.285641   | 0.449812   | 344  | 281   | 625                                   | 625  |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 211.525  | 253.885   | 0.423602   | 0.162172   | 679  | 131   | 810                                   | 810  |
| 137.8                            | 204.314  | 237.697   | 0.33383  | 0.42318  | 410  | 300   | 710                                   | 710  |
| 167.3                            | 19.711   | 226.556   | 0.294453   | 0.389204   | 394  | 251   | 645                                   | 645  |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 233.304  | 278.546   | 0.452419   | 0.108278   | 869  | 106   | 975                                   | 975  |
| 137.8                            | 225.012  | 260.079   | 0.350669   | 0.358975   | 545  | 305   | 850                                   | 850  |
| 167.3                            | 221.638  | 252.313   | 0.306753   | 0.330808   | 535  | 265   | 800                                   | 800  |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 257.607  | 315.392   | 0.577846   | 0.0331079  | 1209   | 41  | 1250                                  | 1250   |
| 137.8                            | 25.937   | 302.513   | 0.431427   | 0.116715   | 1016   | 134   | 1150                                  | 1150   |
| 167.3                            | 254.117  | 291.119   | 0.370019   | 0.184194   | 869  | 196   | 1065                                  | 1065   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 256.153  | 328.976   | 0.728229   | 0.00624113   | 1352   | 8   | 1360                                  | 1360   |
| 137.8                            | 265.994  | 319.154   | 0.531601   | 0.0953393  | 1158   | 122   | 1280                                  | 1280   |
| 167.3                            | 267.211  | 312.222   | 0.450103   | 0.0913077  | 1113   | 112   | 1225                                  | 1225   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 272.392  | 366.723   | 0.943309   | 0.000722156  | 1689   | 1   | 1690                                  | 1690   |
| 137.8                            | 285.735  | 353.464   | 0.677288   | 0.0323153  | 1519   | 51  | 1570                                  | 1570   |
| 167.3                            | 285.255  | 342.022   | 0.567666   | 0.0319982  | 1423   | 47  | 1470                                  | 1470   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 272.005  | 36.618  | 0.941755   | 0.000604864  | 1684   | 1   | 1685                                  | 1685   |
| 137.8                            | 290.321  | 357.938   | 0.676173   | 0.0323153  | 1558   | 52  | 1610                                  | 1610   |
| 167.3                            | 289.971  | 346.644   | 0.566731   | 0.0319982  | 1462   | 48  | 1510                                  | 1510   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 254.198  | 41.122  | 157.022  | 1.6668*10 <sup>-6</sup>  | 2125   | 0   | 2125                                  | 2125   |
| 137.8                            | 295.942  | 406.843   | 110.901  | 0.00126874   | 2077   | 3   | 2080                                  | 2080   |
| 167.3                            | 314.889  | 406.843   | 0.919543   | 0.00136031   | 2077   | 3   | 2080                                  | 2080   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 265.792  | 422.672   | 15.688   | 1.2094*10 <sup>-6</sup>  | 2245   | 0   | 2245                                  | 2245   |
| 137.8                            | 302.832  | 413.632   | 1.108  | 0.00126874   | 2147   | 3   | 2150                                  | 2150   |
| 167.3                            | 321.761  | 413.632   | 0.918711   | 0.00136031   | 2147   | 3   | 2150                                  | 2150   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 272.861  | 429.674   | 156.813  | 1.2008*10-6  | 2320   | 0   | 2320                                  | 2320   |
| 137.8                            | 312.389  | 423.142   | 110.753  | 0.00126874   | 2247   | 3   | 2250                                  | 2250   |
| 167.3                            | 324.676  | 416.508   | 0.918316   | 0.00136031   | 2177   | 3   | 2180                                  | 2180   |
|                                  |  |   |  |  |  |   |                                       |  |
| 96.4                             | 269.673  | 426.421   | 156.747  | 1.2005*10-6  | 2285   | 0   | 2285                                  | 2285   |
| 137.8                            | 310.551  | 421.257   | 110.707  | 0.00126874   | 2227   | 3   | 2230                                  | 2230   |
|                                  | E <sub>L</sub> (MeV)<br>He (2,3) 96.4 137.8 96.4 137.8 167.3 96.4 | L(MeV)<br>He (2,3)r2(fm)<br>He (2,3)96.4213.126137.8198.812167.3194.45196.4211.525137.8204.314167.319.71196.4233.304137.8225.012167.3221.63896.4255.012167.325.937167.325.937167.3256.153137.8265.994167.3265.153137.8265.994167.3285.735167.3285.735167.3285.735167.3285.735167.3289.97196.4272.005137.8290.321167.3289.97196.4272.005137.8290.321167.3314.889137.8302.832167.3321.76196.4272.861137.8302.832167.3324.67696.4272.861137.8312.389167.3324.676 | F_L(MeV)<br>He (2,3)r_2(fm)<br>r_1(fm)96.4213.126253.101137.8198.812230.905167.3194.451223.01696.4211.525253.885137.8204.314237.697167.319.711226.55696.4233.304278.546137.8225.012260.079167.3221.638252.31396.4257.607315.392137.825.937302.513167.3254.117291.11996.4256.153328.976137.8265.994319.154167.3267.211312.22296.4272.392366.723137.8285.735353.464167.3285.255342.02296.4272.00536.618137.8290.321357.938167.3289.971346.64496.4275.052422.672137.8290.321357.938167.3314.889406.843167.3314.889406.843167.3324.761413.63296.4275.861429.674137.8302.832413.632167.3324.676416.50896.4272.861429.674137.8312.389423.142167.3324.676416.50896.4278.861429.674137.8312.389423.142167.3324.676416.50896.4265.792426.421 <td>FL(MeV)<br/>He (2,3)r2(fm)r1(fm)d2 (fm)96.4213.126253.1010.399748137.8198.812230.9050.320928167.3194.451223.0160.28564196.4211.525253.8850.423602137.8204.314237.6970.33383167.319.711226.5560.29445396.4233.304278.5460.452419137.8225.012260.0790.350669167.3221.638252.3130.30675396.4257.607315.3920.577846137.825.937302.5130.431427167.3254.117291.1190.37001996.4256.153328.9760.728229137.8265.994319.1540.531601167.3267.211312.2220.45010396.4272.392366.7230.943309137.8285.735353.4640.677288167.3285.255342.0220.56766696.4272.00536.6180.941755137.8290.321357.9380.676173167.3289.971346.6440.56673196.4254.19841.122157.022137.8295.942406.843110.901167.3314.889406.8430.919543167.3321.761413.6320.91871196.4265.792422.67215.688137.8302.832413.6321.108167.3321.761<!--</td--><td><math>F_{L}(MeV)</math><br/>He (2,3)<math>r_{2}(fm)</math><math>r_{1}(fm)</math><math>d_{2}(fm)</math><math>T(d_{2})</math>96.4213.126253.1010.3997480.349472137.8198.812230.9050.3209280.489133167.3194.451223.0160.2856410.44981296.4211.525253.8850.4236020.162172137.8204.314237.6970.333830.42318167.319.711226.5560.2944530.38920496.4233.304278.5460.4524190.108278137.8225.012260.0790.3506690.358975167.3221.638252.3130.4314270.116715167.3221.638252.3130.4314270.116715167.325.937302.5130.4314270.116715167.3256.153328.9760.7282290.00624113137.8265.994319.1540.5316010.0953393167.3285.735353.4640.6772880.032153167.3285.735353.4640.6772880.032153167.3289.971346.6440.5667310.031998296.4272.00536.6180.9417550.000604864137.8290.321357.9380.6761730.032153167.3289.971346.6440.5667310.031998296.4255.792422.67215.6881.2094*10<sup>6</sup>137.8295.942406.843110.9010.00126874167.3321.761413.632</td><td><math>E_{1}</math>(MeV)<br/>He (2,3)<math>r_{2}</math>(fm)<math>r_{1}</math>(fm)<math>d_{2}</math> 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       198.812         230.905         0.320928         0.489133         342         328         670           167.3         194.451         223.016         0.285641         0.449812         344         281         625           96.4         211.525         253.885         0.423602         0.162172         679         131         810           137.8         204.314         237.697         0.33383         0.42318         410         300         710           167.3         19.711         226.556         0.294453         0.389204         394         251         645           96.4         233.304         278.546         0.452419         0.108278         869         106         975           137.8         252.012         260.079         0.350669         0.331079         1209         41         1250           137.8         257.607         315.392         0.577846         0.0331079         1209         41         1250           167.3</td></t<></td></td> | FL(MeV)<br>He (2,3)r2(fm)r1(fm)d2 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(2,3)<math>r_{2}(fm)</math><math>r_{1}(fm)</math><math>d_{2}(fm)</math><math>T(d_{2})</math>96.4213.126253.1010.3997480.349472137.8198.812230.9050.3209280.489133167.3194.451223.0160.2856410.44981296.4211.525253.8850.4236020.162172137.8204.314237.6970.333830.42318167.319.711226.5560.2944530.38920496.4233.304278.5460.4524190.108278137.8225.012260.0790.3506690.358975167.3221.638252.3130.4314270.116715167.3221.638252.3130.4314270.116715167.325.937302.5130.4314270.116715167.3256.153328.9760.7282290.00624113137.8265.994319.1540.5316010.0953393167.3285.735353.4640.6772880.032153167.3285.735353.4640.6772880.032153167.3289.971346.6440.5667310.031998296.4272.00536.6180.9417550.000604864137.8290.321357.9380.6761730.032153167.3289.971346.6440.5667310.031998296.4255.792422.67215.6881.2094*10<sup>6</sup>137.8295.942406.843110.9010.00126874167.3321.761413.632</td> <td><math>E_{1}</math>(MeV)<br/>He (2,3)<math>r_{2}</math>(fm)<math>r_{1}</math>(fm)<math>d_{2}</math> (fm)<math>T(d_{2})</math><math>\sigma_{s}^{cal}</math><br/>(mb)96.4213.126253.1010.3997480.349472524137.8198.812230.9050.3209280.489133342167.3194.451223.0160.2856410.44981234496.4211.525253.8850.4236020.162172679137.8204.314237.6970.333830.42318410167.319.711226.5560.2944530.38920439496.4233.304278.5460.4524190.108278869137.8225.012260.0790.3506690.358975545167.3221.638252.3130.3067530.3308085596.4257.607315.3920.5778460.03310791209137.825.937302.5130.4314270.1167151016167.3254.117291.1190.3700190.184194869996.4256.153328.9760.7282290.006241131352137.8265.994319.1540.5316010.09533931158167.3285.255342.0220.5676660.031982142396.4272.392366.7230.9433090.0007221561689137.8285.735353.4640.6772880.03231531519167.3285.255342.0220.5676660.031982142396.4272.00536.618<t< td=""><td></td><td>He (2,3)         (mb)         (mb)         (mb)         (mb)         (mb)           96.4         213.126         253.101         0.399748         0.349472         524         281         805           137.8         198.812         230.905         0.320928         0.489133         342         328         670           167.3         194.451         223.016         0.285641         0.449812         344         281         625           96.4         211.525         253.885         0.423602         0.162172         679         131         810           137.8         204.314         237.697         0.33383         0.42318         410         300         710           167.3         19.711         226.556         0.294453         0.389204         394         251         645           96.4         233.304         278.546         0.452419         0.108278         869         106         975           137.8         252.012         260.079         0.350669         0.331079         1209         41         1250           137.8         257.607         315.392         0.577846         0.0331079         1209         41         1250           167.3</td></t<></td> | $F_{L}(MeV)$<br>He (2,3) $r_{2}(fm)$ 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$\sigma_{s}^{cal}$<br>(mb)96.4213.126253.1010.3997480.349472524137.8198.812230.9050.3209280.489133342167.3194.451223.0160.2856410.44981234496.4211.525253.8850.4236020.162172679137.8204.314237.6970.333830.42318410167.319.711226.5560.2944530.38920439496.4233.304278.5460.4524190.108278869137.8225.012260.0790.3506690.358975545167.3221.638252.3130.3067530.3308085596.4257.607315.3920.5778460.03310791209137.825.937302.5130.4314270.1167151016167.3254.117291.1190.3700190.184194869996.4256.153328.9760.7282290.006241131352137.8265.994319.1540.5316010.09533931158167.3285.255342.0220.5676660.031982142396.4272.392366.7230.9433090.0007221561689137.8285.735353.4640.6772880.03231531519167.3285.255342.0220.5676660.031982142396.4272.00536.618 <t< td=""><td></td><td>He (2,3)         (mb)         (mb)         (mb)         (mb)         (mb)           96.4         213.126         253.101         0.399748         0.349472         524         281         805           137.8         198.812         230.905         0.320928         0.489133         342         328         670           167.3         194.451         223.016         0.285641         0.449812         344         281         625           96.4         211.525         253.885         0.423602         0.162172         679         131         810           137.8         204.314         237.697         0.33383         0.42318         410         300         710           167.3         19.711         226.556         0.294453         0.389204         394         251         645           96.4         233.304         278.546         0.452419         0.108278         869         106         975           137.8         252.012         260.079         0.350669         0.331079         1209         41         1250           137.8         257.607         315.392         0.577846         0.0331079         1209         41         1250           167.3</td></t<> |                                       | He (2,3)         (mb)         (mb)         (mb)         (mb)         (mb)           96.4         213.126         253.101         0.399748         0.349472         524         281         805           137.8         198.812         230.905         0.320928         0.489133         342         328         670           167.3         194.451         223.016         0.285641         0.449812         344         281         625           96.4         211.525         253.885         0.423602         0.162172         679         131         810           137.8         204.314         237.697         0.33383         0.42318         410         300         710           167.3         19.711         226.556         0.294453         0.389204         394         251         645           96.4         233.304         278.546         0.452419         0.108278         869         106         975           137.8         252.012         260.079         0.350669         0.331079         1209         41         1250           137.8         257.607         315.392         0.577846         0.0331079         1209         41         1250           167.3 |

Table 2. [He [2,3] + Xn [Z,N] Cross-sections comparison with those measured (case 2)

| Sn (50,120) | 167.3 | 324.715 | 416.508 | 0.917934 | 0.00136031               | 2177 | 3 | 2180 | 2180 |
|-------------|-------|---------|---------|----------|--------------------------|------|---|------|------|
|             |       |         | 1       |          |                          |      |   |      |      |
| Sn (50,124) | 96.4  | 274.438 | 431.061 | 156.623  | 1.2074*10-6              | 2335 | 0 | 2335 | 2335 |
| Sn (50,124) | 137.8 | 309.693 | 420.312 | 110.619  | 0.00126874               | 2217 | 3 | 2220 | 2220 |
| Sn (50,124) | 167.3 | 322.872 | 414.593 | 0.917206 | 0.00136031               | 2157 | 3 | 2160 | 2160 |
|             |       |         |         |          |                          |      |   |      |      |
| Pb (82,208) | 96.4  | 218.335 | 469.075 | 250.741  | 1.4303*10 <sup>-10</sup> | 2765 | 0 | 2765 | 2765 |
| Pb (82,208) | 137.8 | 300.165 | 476.231 | 176.066  | 9.5459*10 <sup>-6</sup>  | 2850 | 0 | 2850 | 2850 |
| Pb (82,208) | 167.3 | 328.314 | 473.718 | 145.403  | 0.00001124               | 2820 | 0 | 2820 | 2820 |

# When Tables 1 and 2 Are Examined, The Following Can Be Said:

It is not necessary to know the exact form of the  $U_3$  potential segment in the calculation of the scattering cross sections. It doesn't matter where the coordinate start is taken. There is no need to calculate wave functions. It is sufficient to find the width of the barrier potential causing the scattering and the distance from the potential center of the point where the incoming current touches the potential barrier. Thus, it becomes very easy to calculate the scattering cross sections.

Sn(50, 112 - 124) nuclear nuclei are a very good barrier for the energy 96.4 MeV of incoming current, and Pb(82, 208) nuclear nuclei for all three-energy of incoming current.

# WHEN THE SCATTERING CROSS-SECTIONS ARE KNOWN, THE CALCULATION OF THE BARRIER WIDTH AND BARRIER TRANSMISSION COEFFICIENT

By measuring the scattering cross sections, the width of the potential barrier and the transmission coefficient of barrier can be calculated. From equations (20-22), we get the following values:

$$r_1 = \frac{\sqrt{\sigma_r + \sigma_s}}{2\sqrt{10 \pi}} ;$$

$$T = \frac{\sigma_r}{\sigma_r + \sigma_s} ;$$

$$r_2 = r_1 - \frac{\operatorname{arccosh}\left[(2 - T)/T\right]}{2 \text{ K} * 10^{13}}$$
;

$$d_2(E_r) = \frac{\operatorname{arccosh} \left[ (2 - T)/T \right]}{2 \text{ K} * 10^{13}}$$

In these equations, the desired values are obtained by taking the experimentally measured crosssections:

 $T(d_2(E_r)) = \frac{\sigma_r^{exp}}{\sigma_r^{exp} + \sigma_s^{exp}}, \text{ obstacle passing coefficient ; } d_2(E_r) = \frac{\arccos \left[ (2-T)/T \right]}{2 \text{ K} * 10^{13}}, \text{ Obstacle width. The barrier potential widths and barrier transmission coefficients calculated for many thermal neutron cross sections are given in Table 3. Experimental cross section values were taken from [9].}$ 

| Neucleus    | σsexp | $\sigma_R^{exp}$ | $\sigma_T^{exp}$ | $\mathbf{r}_2$ | $\mathbf{r}_1$ | <b>d</b> <sub>2</sub>    | T (d <sub>2</sub> ) |
|-------------|-------|------------------|------------------|----------------|----------------|--------------------------|---------------------|
| Xn (Z, N)   | (mb)  | (mb)             | (mb)             | ( <b>fm</b> )  | (fm)           | ( <b>fm</b> )            |                     |
| n (0,1)     | 20491 | 332.6            | 20823.6          | 12.8728        | 12.8728        | 1.58781x10 <sup>-8</sup> | 0.015972            |
| H (1,1)     | 20491 | 332.6            | 20823.6          | 12.8728        | 12.8728        | 1.58781x10 <sup>-8</sup> | 0.015972            |
| H (1,2)     | 3390  | 0.519            | 3390.52          | 5.19431        | 5.19431        | 2.93019x10 <sup>-8</sup> | 0.000153            |
| Be (4,9)    | 6151  | 7.6              | 6158.6           | 7.00061        | 7.00061        | 1.74644x10 <sup>-8</sup> | 0.001234            |
| C (6,12)    | 4746  | 3.53             | 4749.53          | 6.14781        | 6.14781        | 1.37499x10 <sup>-8</sup> | 0.000743            |
| 0 (8,16)    | 3761  | 0.19             | 3761.19          | 5.47089        | 5.47089        | 1.76016*10 <sup>-8</sup> | 0.000051            |
| Si (14,28)  | 1992  | 177              | 2169             | 4.15456        | 4.15456        | 5.89164x10 <sup>-9</sup> | 0.081604            |
| Ca (20,40)  | 3010  | 410              | 3420             | 5.21685        | 5.21685        | 5.13741x10 <sup>-9</sup> | 0.119883            |
| Ni (28,58)  | 25300 | 4600             | 29900            | 15.4252        | 15.4252        | 4.6877x10 <sup>-9</sup>  | 0.153846            |
| Ni (28,60)  | 980   | 2900             | 3880             | 5.55662        | 5.55662        | 1.61904x10 <sup>-9</sup> | 0.747423            |
| Sn (50,112) | 4909  | 626              | 5535             | 6.63673        | 6.63673        | 5.13281x10 <sup>-9</sup> | 0.113098            |
| Sn (50,114) | 4600  | 115              | 4715             | 6.12542        | 6.12542        | 7.38953x10 <sup>-9</sup> | 0.024390            |
| Sn (50,118) | 4260  | 220              | 4480             | 5.97082        | 5.97082        | 6.3536x10 <sup>-9</sup>  | 0.049107            |
| Sn (50,120) | 5170  | 140              | 5310             | 6.50043        | 6.50043        | 7.27166x10 <sup>-9</sup> | 0.026365            |
| Sn (50,124) | 4410  | 134              | 4544             | 6.01332        | 6.01332        | 7.10577x10 <sup>-9</sup> | 0.029489            |
| Te (52,124) | 3800  | 6800             | 10600            | 9.18434        | 9.18434        | 2.00611x10 <sup>-9</sup> | 0.641509            |
| Ba (56,130) | 3420  | 1200             | 4620             | 6.0634         | 6.0634         | 3.75812x10 <sup>-9</sup> | 0.259740            |
| Ce 58,140)  | 2830  | 570              | 3400             | 5.20157        | 5.20157        | 4.47176x10 <sup>-9</sup> | 0.167647            |
| Nd 60,142)  | 7700  | 18700            | 26400            | 14.4943        | 14.4943        | 1.75215x10 <sup>-9</sup> | 0.708333            |
| Nd 60,148)  | 4000  | 2500             | 6500             | 7.19203        | 7.19203        | 3.06436x10 <sup>-9</sup> | 0.384615            |

Table 3. [n (0, 1) + Xn (Z, N)], when the scattering cross-sections are known, the calculation of the barrier width and barrier transmission coefficient for thermal neutrons.

When Table 3 is examined, it can be seen that  $d_2 \neq 0$  and  $T \neq 1$  are for thermal neutrons, although  $r_1 = r_2$ . This situation can be explained as follows: (1) The calculation of  $r_1$  ve  $r_2$  may be due to their precession. (2) There may be a barrier potential other than the centrifugal potential in the structure of the target nuclei.

# CONCLUSION

The calculation of cross sections through solution of radial SE (RSE) by the partial wave expansion is exceedingly difficult. In many cases, some approximations are needed for these kinds of solutions. For these reasons, there is no simple scattering cross-section formula. However, here, simple scattering cross-section formulas were obtained without any approximation. These formulas will provide great convenience to those who do research on these issues. It will provide great convenience especially in material physics research. Examples here are taken from nuclear physics, but this method can also be used in other branches of physics. In the present study, firstly, differential elastic scattering, inelastic (or reaction) scattering and total cross-sections have been calculated without using any approximation. These calculations have been performed using a simple method, improved for the solution of RSE, for an incident particle being in a central field of any form. We have obtained the general formulas of the scattering amplitudes and elastic, inelastic (no-elastic) and total scattering cross-sections. Secondly, we have made some applications. In these applications, the potentials have been assumed to have two shapes plus centrifugal and Coulomb potentials. Calculations with these are not easy by the partial wave expansion. However, it is guite easy to make calculations with our method. With these potentials, the elastic, inelastic (neutron radiative capture, etc.), and total scattering cross-sections of different targets have been calculated. The calculated results have been compared with experimental results. The results calculated have given satisfactory agreement with the available

experimental results. Then, when the experimental elastic and reaction cross sections are known, we calculated the width of the potential barrier and the coefficient of transmission the potential barrier. By taking thermal neutrons as incoming particles, the potential barrier transmission coefficients and barrier widths were calculated for many nuclei.

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